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Article

Rejuvenation of Zr-Based Bulk Metallic Glasses by Ultrasonic Vibration-Assisted Elastic Deformation

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Abstract: The rejuvenation of $Zr_{52.5}Cu_{17.9}Ni_{14.6}Al_{10}Ti_5$ bulk metallic glasses (BMGs) by ultrasonic vibration-assisted elastic deformation (UVEF) was studied herein. The UVEF-treated samples demonstrate an obvious rejuvenation and have a higher relaxation enthalpy and a smaller range of supercooled liquid regions than the as-cast samples. The fracture of the rejuvenated amorphous alloy is mainly ductile fracture, and shear deformation occurs in the deformation region. It is also found that as the amplitude increases, the free volume of the rejuvenated amorphous alloy increases, the yield strength and the elastic modulus decrease, and the formability increases. The free-volume content is used to characterize the degree of rejuvenation, and a mathematical model of the relationship between the ultrasonic amplitude and free volume is established. In addition, it is found that the ultrasonic vibration stress induces the additional free volume in the Zr-based bulk metallic glasses and improves the plasticizing behavior. The temperature rise caused by the ultrasonic thermal e ect does not induce additional free volume.

Keywords: bulk metallic glasses (BMGs); rejuvenation; ultrasonic vibration-assisted elastic deformation (UVEF); free volume; plasticity

1. Introduction

Bulk metallic glasses (BMGs) are materials with excellent performance and mechanical properties, such as high yield strength [1], high toughness [2], high hardness [3] and exceptional “damage tolerance” [4,5]. However, the nonuniform deformation caused by the highly localized deformation at room temperature directly causes its brittleness [6,7], which has become the bottleneck for the widespread application of BMGs. Reducing the brittleness of BMGs has become a scientific issue that scholars have begun to pay attention to.

The rejuvenation of amorphous alloys occurs when BMGs are injected with high energy because it endows them with additional free volume and greater plasticity [8,9]. Therefore, rejuvenation of BMGs to reduce their brittleness and improve their plasticity at room temperature has attracted a lot of attention [10–12]. For example, J. Michler [13] conducted compression experiments on ion-radiated BMGs and found that they can increase the free-volume content of BMGs and enhance their plasticity. J. Das [14] utilized cold-rolled Zr-based BMGs at room temperature to overcome their inherent brittleness and make BMGs plastic from 0.5% to 15%. F. X. Li [15] discovered that during the elastic compression of $Zr_{35}Ti_{30}Be_{27.5}Cu_{7.5}$ BMGs at room temperature, the BMGs transitioned from mechanical relaxation to rejuvenation, thereby improving their plasticity. W. Guo [16] studied the rejuvenation of Zr–Cu–Al–Ni–Ta BMGs under cryogenic cycle treatment (DCT) and found that by adding more Ta, the BMGs can be restored to an elevated energy, and the compressive fracture strength and plastic strain increased with increasing Ta content. Through plastic deformation under triaxial compression at room temperature,

Y. Li and A.L. Greer [4] rejuvenated BMGs samples and found that the rejuvenated amorphous material showed excellent plastic deformation ability. However, elastic loading [17], ion radiation [18], thermal cycling [19,20], and plastic deformation [21] methods require a substantial amount of time to rejuvenate the BMGs, and during this time, a relaxation effect inevitably occurs, weakening the rejuvenation effect.

In addition, ultrasonic vibration-assisted has an ultrasonic stress e ect and ultrasonic thermal e ect. P. Chen [22] used ultrasonic vibration to process a Ti-based amorphous powder to make nanocrystalline bulk materials. The amorphous powder was crystallized by the frictional heat generated during the ultrasonic vibration and then welded to form a bulk nanocrystalline material. J. Ma et al. [23] used supersonic vibration to stamp BMGs and found that this forming method completed thermoplastic forming in seconds and largely avoided the time-dependent crystallization and oxidation processes, thus avoiding the risk of crystallization that occurs during traditional heat processing. N. Li et al. [24] conducted uniaxial tensile and compression experiments on Zr-based amorphous alloys under the action of a vibration field and found that with increasing vibration frequency, the free-volume content of the amorphous alloy increased and the flow unit volume decreased, which caused the flow viscosity to decrease and the micro-forming ability to increase. However, there are no reports that specifically analyze the influence of ultrasonic vibration stresses and ultrasonic thermal e ects on amorphous properties.

A novel method of ultrasonic vibration-assisted elastic deformation (UVEF) was developed that can successfully and rapidly rejuvenate Zr-based BMGs within 8 s. It was found that ultrasound-assisted vibration can rapidly increase the internal energy of BMGs and quickly drive the loosely packed atoms in BMGs to high-energy regions, thereby driving additional areas with free volume and rheological units to form shear bands. These processes result in the rapid rejuvenation of BMGs and prevent the time-dependent crystallization and relaxation phenomena. In addition, the thermodynamics, mechanical properties and fracture morphology of the rejuvenated UVEF-treated samples were analyzed. It was found that as the amplitude increased, the yield strength and elastic modulus of the UVEF-treated samples decreased, and the plasticity was greatly improved. The free volume was used to characterize the degree of rejuvenation of the amorphous alloys herein, and a mathematical model of the relationship between the ultrasonic amplitude and the free volume of the rejuvenated BMGs was established. The e ects of the temperature rise and stress caused by the ultrasonic vibration on the rejuvenation properties of BMGs were analyzed. These findings provide a convenient and fast method to reduce the room-temperature brittleness of BMGs and improve their plasticity.

2. Experimental Methods

2.1. Sample Preparation

The experimental material is an amorphous alloy with an alloy composition of $Zr_{52.5}Cu_{17.9}Ni_{14.6}Al_{10}Ti_5$ (atomic percentage). The raw materials of metals Zr, Cu, Ni, Al, and Ti with a purity of 99.9% or more are prepared according to the nominal composition. An electric arc furnace is used to melt the master alloy, and then a copper die suction casting method is used to prepare rod-shaped amorphous particles with a diameter of F 2 mm. A low-speed diamond cutting machine is used to process a cylindrical sample with dimensions of F 2 mm 4 mm. The ends of the cylinder are also polished to ensure that both ends are parallel to each other and orthogonal to the centerline of the cylinder. The sample was analyzed with X-ray di raction (XRD, Bruker D8 Advance, Bruker, Karlsruhe, Germany) to ensure that the sample is in an amorphous state.

2.2. UVEF Processing

The experiments herein use a homemade ultrasonic vibration-assisted compression test platform. The ultrasonic vibration-assisted device is installed on a Zwick Z050 tensile testing machine (Zwick Roell Group, Ulm, Germany). The maximum power of the ultrasonic system is 1500 W, and the vibration frequency is 20 kHz. Due to the limitation of the experimental conditions, the ultrasonic frequency in

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UVEF can be calculated:

$$t = t_{pl} + t_{ul} = \frac{S_{pl}}{V_{tp}} + \frac{\varepsilon}{\dot{\varepsilon}} \quad (1)$$

where t_{pl} is the time of preloading, t_{ul} is the ultrasonic loading time, S_{pl} is the distance between the initial punch and the upper surface of the sample, and V_{tp} is the preloading speed. S_{pl} and V_{tp} were taken as 0.5 mm and 0.1 mm/s, respectively. A strain rate of $\dot{\varepsilon}$ = 0.01 s^{-1} and a strain of ε = 2% were were taken as 0.5 mm and 0.1 mm/s, respectively. A strain rate of 0.01 s^{-1} and a strain of 2% applied toensure ensurethatcompressionthatcompressionisthinisthewithinamorphousamorphouselasticdeformationelasticdeformationrange,andrange,BMGs andcan beBMGsrejuvenatedcanatbedrejuvenatedwithin8s. Five BMGs8s. samples FiveBMGswere samplesreeatedlywerecompressedrepeatedly under compressedachdeformationundereach process deformation condition process condition.

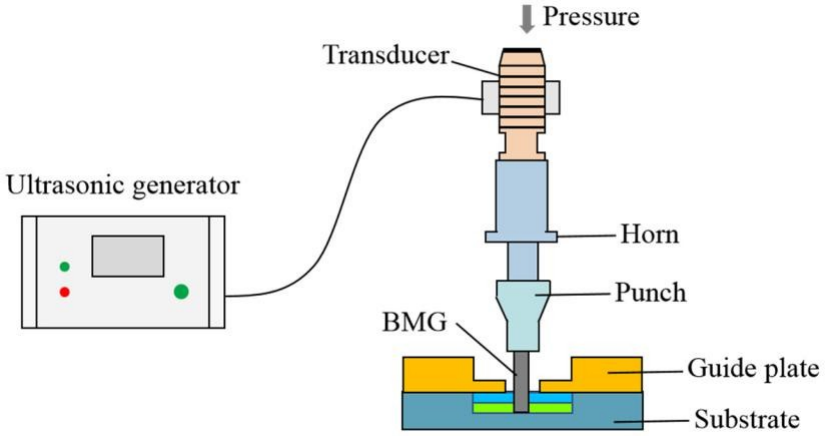

Figure 1.. Ultrasonic vibration--assisted elastic deformation diagram.

2.3. Hot-Compressed Elastic Deformation (HEF) Experiment

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To specialized analyze the e cts of the temperature rise and stress produced during the ultrasonic To specialized analyze the effects of the temperature rise and stress produced during the vibration on the rejuvenation properties of the amorphous alloys, we eliminate the e ect of ultrasonic ultrasonic vibration on the rejuvenation properties of the amorphous alloys, we eliminate the effect stress, and only the e ect of temperature rise is studied separately. The temperature rise at di erent of ultrasonic stress, and only the effect of temperature rise is studied separately. The temperature rise amplitudes is obtained according to previous research results [25]. That is, amplitudes of 19, 27, 36, at different amplitudes is obtained according to previous research results [25]. That is, amplitudes of and 43 m correspond to temperature increases of 80, 150, 200, and 270 C. HEF experiments at the 19, 27, 36, and 43 μm correspond to temperature increases of 80, 150, 200, and 270 °C. HEF corresponding temperatures are performed on the thermal simulation machine (Gleeble3800, DSI, experiments at the corresponding temperatures are performed on the thermal simulation machine Austin, TX, USA). The corresponding strain rate and strain are consistent with the UVEF experiment (Gleeble3800, DSI, Austin, TX, USA). The corresponding strain rate and strain are consistent with the and are 0.01 s^{-1} and 2%, respectively. Five BMGs samples are repeatedly hot-compressed under each UVEF experiment and are 0.01 s^{-1} and 2%, respectively. Five BMGs samples are repeatedly hot- deformation condition.

compressed under each deformation condition.

2.4. Analytical Testing

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To study the properties of the Zr-based BMGs samples, a series of analytical tests are performed on To study the properties of the Zr-based BMGs samples, a series of analytical tests are performed them. XRD (Bruker D8 Advance, Bruker, Karlsruhe, Germany) is used to determine the crystallization on them. XRD (Bruker D8 Advance, Bruker, Karlsruhe, Germany) is used to determine the of the samples. The scanning range is 20 ~80 , the step size is 0.02 step 1, and the scanning speed is crystallization of the samples. The scanning range is 20° ~ 80°, the step size is 0.02°·step−1, and the 12 min 1. The Vickers microhardness test (BUEHLER 5103, Buehler, Lake Blu , IL, USA; ASTM 92-82, scanning speed is 12°·min−1. The Vickers microhardness test (BUEHLER 5103, Buehler, Lake Bluff, IL,

USA; ASTM E92-82, West Conshohocken, PA, USA) is used to determine the hardness of the samples, the diamond indenter was pressed into the surface of the specimen along its axial direction with a

force of 50 gf, and then the force was held for 10 s. Differential scanning calorimetry (DSC, PerkinElmer DSC8000, PerkinElmer, Poulsbo, WA, USA) is used to analyze the hermodynamic characteristics of the samples at a heating temperature of 520 °C, and the heating and cooling rates are 20 °C min $^{-1}$. Transmission electron microscopy (TEM, JEM-2100F, JEOL Ltd., Tokyo, Japan) with an acceleration voltage of 200 kV is used to observe the microstructure of the samples. The thin foil samples for TEM observation are cut from 0.5 mm grid. The thinning procedures were performed by alternately milling both sides of the lamina with a tilt angle of ±1.2°. The thickness of the lamina was reduced within 100 nm. The Ga ion energy was 30 kV and a current of 0.1 nA. The quasi-static compression test is used to determine the plasticity, yield strength and elastic modulus of the samples. The strength experiments are carried out on a Zwick Z050 universal tensile machine (Zwick Roell Group), and the strain rate is 0.0005 s $^{-1}$. Scanning electron microscopy (SEM, FEI Quanta 450FEG, FEI Company, Hillsboro, OR, USA) is used to observe the fracture morphology of the quasi-static compression fracture samples. All test experiments are repeated 5 times. All test results are reported herein as the average of 5 repeated samples.

3. Results and Discussion

Figure 2 is a comparison of the XRD patterns of the as-cast and UVEF-treated samples. It can be found that the XRD diffraction peaks of the UVEF-treated samples are consistent with those of the as-cast samples. There are broad diffusion peaks without any obvious crystalline peaks in both cases, which indicates that the as-cast and UVEF-treated samples are all amorphous, and ultrasonic vibration-assisted elastic deformation does not cause the amorphous material to crystallize. Regarding the naming convention, the UVEF-19 sample is an amorphous sample treated by ultrasonic vibration-assisted elastic deformation with an amplitude of 19 μm.

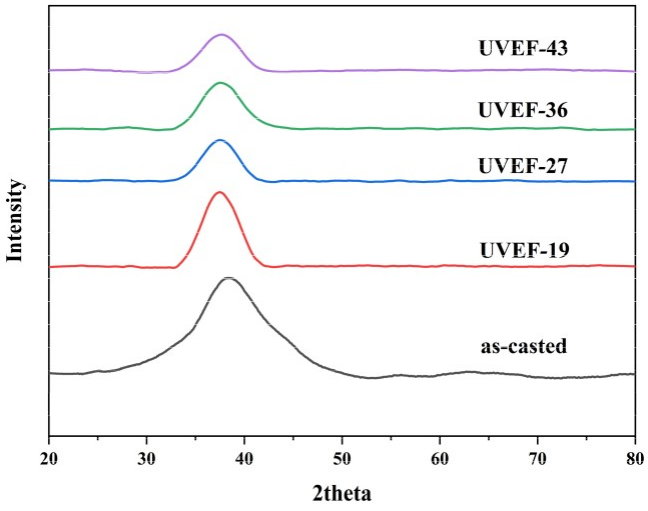

Figure 2. Comparison of the XX-ray-ray diffraction (XRD) (XRD) patterns patterns of the of as the-cas as -and cast ultrasonic and ultrasonic vibration vibration-assisted- assisted elastic deformation lastic deformation (UVEF) -treated (UVEF) samples -treated. samples.

To further confirm confirm the the amorphous properties of the of as the-cast-and cast UVEF and -UVEF treated -treated samples, samples, high- resolution high-resolution TEM is TEM used is to used obtain to obtain an image a no image of the microstructure of the microstructure of the sample, of the which sample, is shown which in is Figure shown 3 in. No Figure nanocrystals 3. No nanocrystals are found are in the found as- cast in he samples as-cast or samples the UVEF or the -treated UVEF sampl -treate s, d samples, and the microstructure and the microstructure of all samples of all shows samples labyrinth shows -like labyrinth characteristics -like characteristics similar to those similar of an to amorphous those of an state, amorphous which state, is consistent which is with consistent the XRD with test the results XRD. test results.

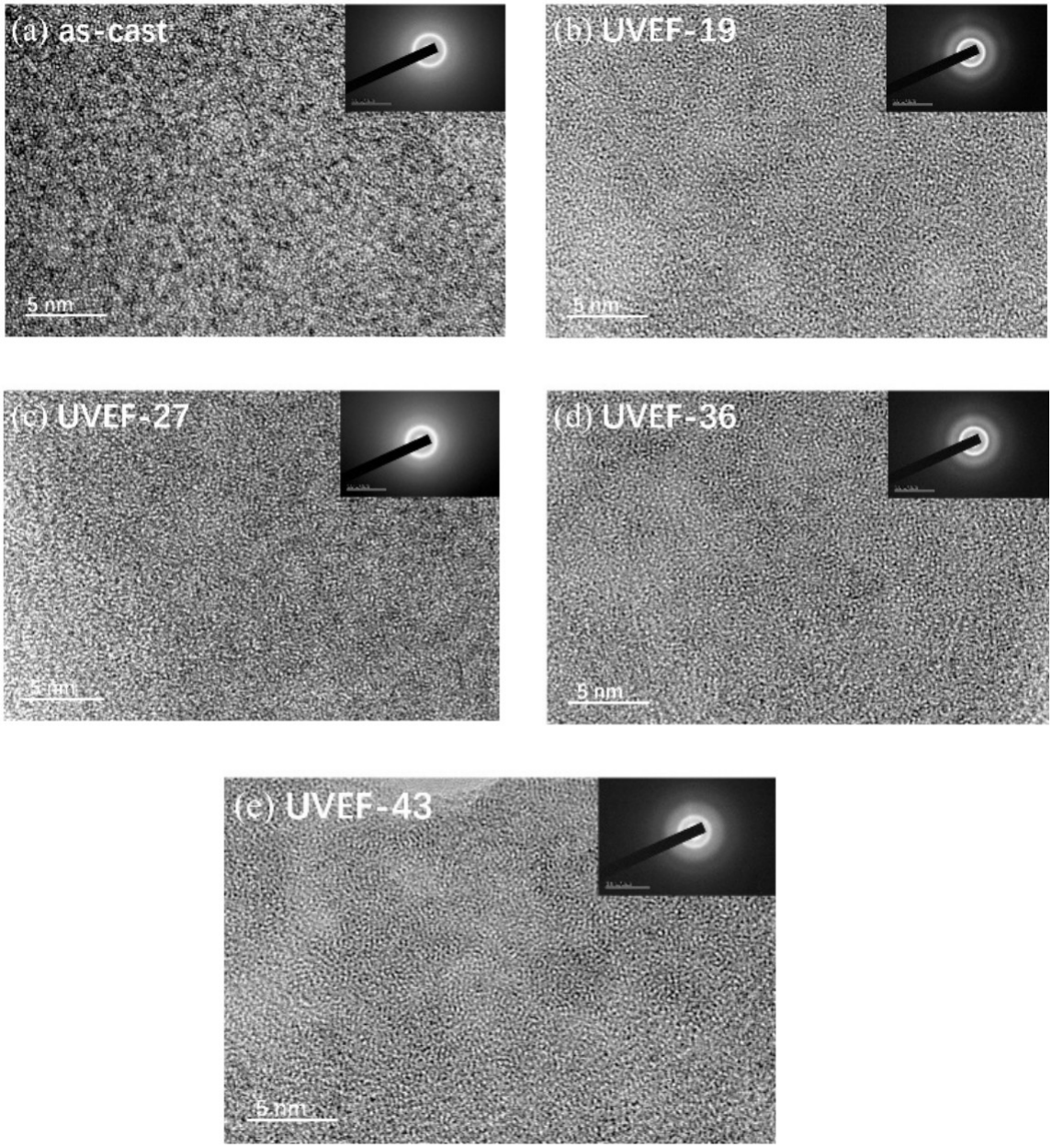

Figure 3. Transmission electron microscopy (TEM)) images of the as-cast sample and the UVEF-treated **Figure 3.** Transmission electron microscopy (TEM)) images of the as-cast sample and the UVEF- samples: (**a**) as-cast; (**b**) UVEF-19; (**c**) UVEF-27; (**d**) UVEF-36; and (**e**) UVEF-43.
treated samples: (**a**) as-cast; (**b**) UVEF-19; (**c**) UVEF-27; (**d**) UVEF-36; and (**e**) UVEF-43.

3.1. Thermodynamics Analysis

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The as-cast and UVEF-treated samples are analyzed by DSC, and the thermodynamic properties The as-cast and UVEF-treated samples are analyzed by DSC, and the thermodynamic properties of the samples are obtained from the DSC curve. As shown in Figure 4, the DSC curves of all samples
of the samples are obtained from the DSC curve. As shown in Figure 4, the DSC curves of all samples show an endothermic phenomenon starting from the T_g temperature, which is a characteristic of glass show an endothermic phenomenon starting from the T_g temperature, which is a characteristic of glass transition, and then exhibit an exothermic phenomenon corresponding to the crystallization behavior
transition, and then exhibit an exothermic phenomenon corresponding to the crystallization behavior to the T_x temperature. The values of T_g and T_x for as-cast and UVEF treated samples as shown in to the T_x temperature. The values of T_g and T_x for as-cast and UVEF treated samples as shown in Table Table 1.
1.

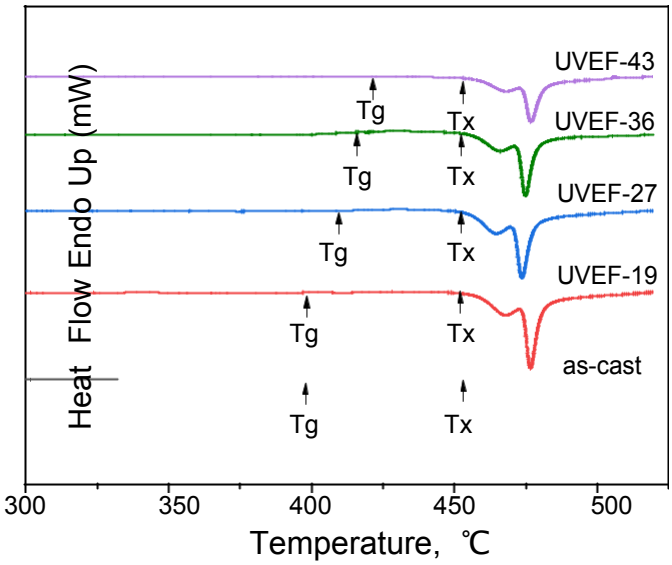


Figure 4. Differential scanning calorimetry (DSC) curves of the as-cast and UVEF-treated samples.
Figure 4. Di erential scanning calorimetry (DSC) curves of the as-cast and UVEF-treated samples.

TableTable1. 1 The.Thevaluesvaluesof ofthetheglassglasstransitiontemperatureTgTandgandthethecrystallizationtemperatureTxTforxfor asas-cast-castandandUVEFtreatedsamples..

Sample	T_g (K)T_g (K)	T_x (K)T_x (K)	DTΔ(K)T(K)
As-cast	397 397	452 452	55
UVEF-19	398 398	452 452	54
UVEF-27	410 410	453 453	43
UVEFUVEF-36-36	416 416	453 453	3737
UVEF-43-43	422 422	454 454	3232

Compared with that of the as-cast sample, the crystallization temperature T_x of the UVEF-treated Compared with that of the as-cast sample, the crystallization temperature Tx of the UVEF-treated sample shows only slight fluctuations, roughly in the range of 453 ± 1 °C, while the glass transition sample shows only slight fluctuations, roughly in the range of 453 1 C, while the glass transition temperature T_g showed an upward trend with increasing ultrasonic amplitude. This shows that an temperature Tg showed an upward trend with increasing ultrasonic amplitude. This shows that increased amplitude ultrasonic vibration can increase the glass transition temperature T_g of the an increased amplitude ultrasonic vibration can increase the glass transition temperature Tg of the amorphous alloy and reduce the range of its supercooled liquid region. According to the Spaepen amorphous alloy and reduce the range of its supercooled liquid region. According to the Spaepen plastic deformation mechanism, BMGs will undergo uneven plastic deformation at high strain rates, plastic deformation mechanism, BMGs will undergo uneven plastic deformation at high strain rates, resulting in a large number of shear bands. The arrangement density of atoms near the shear zone is resulting in a large number of shear bands. The arrangement density of atoms near the shear zone is less than that of the matrix, so a large amount of free volume is concentrated in the shear zone at this less than that of the matrix, so a large amount of free volume is concentrated in the shear zone at this time, causing the increase of atomic mobility, the deterioration of the thermal stability of the material, time, causing the increase of atomic mobility, the deterioration of the thermal stability of the material, and the increase of T_g [8,26].
and the increase of Tg [8,26].

Because of the structural relaxation, the amorphous alloy exhibits exothermic phenomena Because of the structural relaxation, the amorphous alloy exhibits exothermic phenomena during continuous heating to the T_g (Figure 5). The larger the value of free volume change (ΔV_f) is, continuous heating to the Tg (Figure 5). The larger the value of free volume change (DVf) is, the greater the greater the initial free volume (V_f) of the amorphous alloy before heating [27]. Figure 5 shows the the initial free volume (Vf) of the amorphous alloy before heating [27]. Figure 5 shows the relaxation relaxation enthalpy ΔH of the as-cast and UVEF -treated samples during DSC thermodynamic enthalpy DH of the as-cast and UVEF-treated samples during DSC thermodynamic analysis. The DH analysis. The ΔH is calculated by calculating the integrated area of the exothermic peak, and the is calculated by calculating the integrated area of the exothermic peak, and the change in DH reflects change in ΔH reflects the disorder of the atomic arrangement [28]. It is found that with an increase in the disorder of the atomic arrangement [28]. It is found that with an increase in the ultrasonic the ultrasonic amplitude, the ΔH value of the UVEF -treated sample increases significantly. The larger amplitude, the DH value of the UVEF-treated sample increases significantly. The larger the DH value the ΔH value is, the greater the free volume V_f value of the amorphous alloy. This is because under is, the greater the free volume Vf value of the amorphous alloy. This is because under the vibration the vibration load, the UVEF- treated samples were injected with a high energy and the atom diffusion load, the UVEF-treated samples were injected with a high energy and the atom di usion increases. increases. The atomic arrangement also becomes looser, and the larger the amplitude is, the stronger The atomic arrangement also becomes looser, and the larger the amplitude is, the stronger the atom the atom diffusion and the higher the amorphous energy. This result also shows that the degree of di usion and the higher the amorphous energy. This result also shows that the degree of rejuvenation rejuvenation of the UVEF- treated sample increases.
of the UVEF-treated sample increases.

3.4. *Fracture Micrography* shows the compressive fracture micromorphology of the as-cast and UVEF-treated samples obtained by SEM. All samples fracture along the maximum shear stress plane at an angle of approximately 45° to the loading axis. The microstructure was not uniform across the fracture surface, and the fractures of as-cast samples are obviously in the shape of veins, mountains, and rivers (Figure 8a), which is a typical brittle fracture morphology. The fracture surface morphology of the UVEF-treated samples indicates mainly ductile fracture (Figure 8b–e). The fracture surface has a large number of vein-like textures. This texture is due to the shear zone breaking during the stress loading process. The local melting phenomenon caused by the instantaneous release indicates that the material has undergone shear deformation in the region, which is consistent with the experimental results in Figure 6a, indicating that the ultrasonic vibration-assisted elastic deformation process rejuvenates the amorphous alloys.

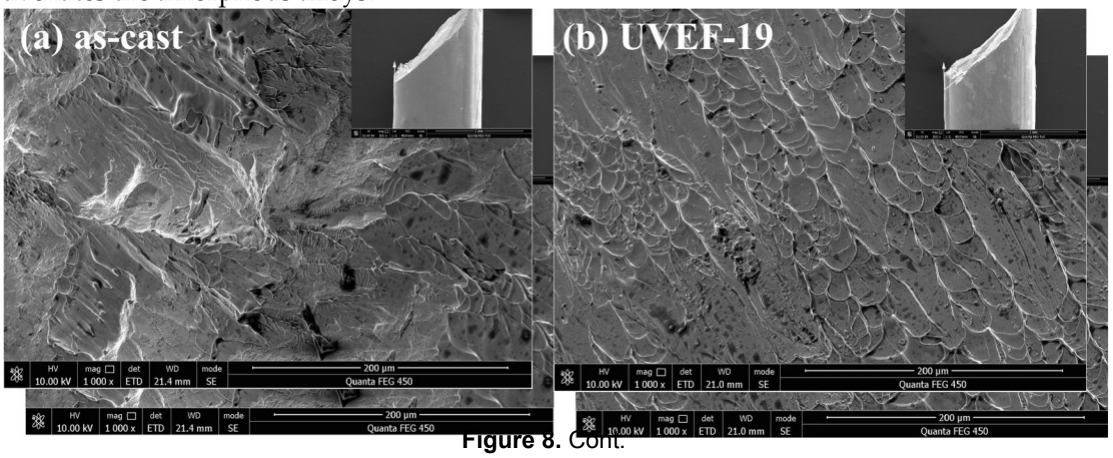


Figure 8. Cont.

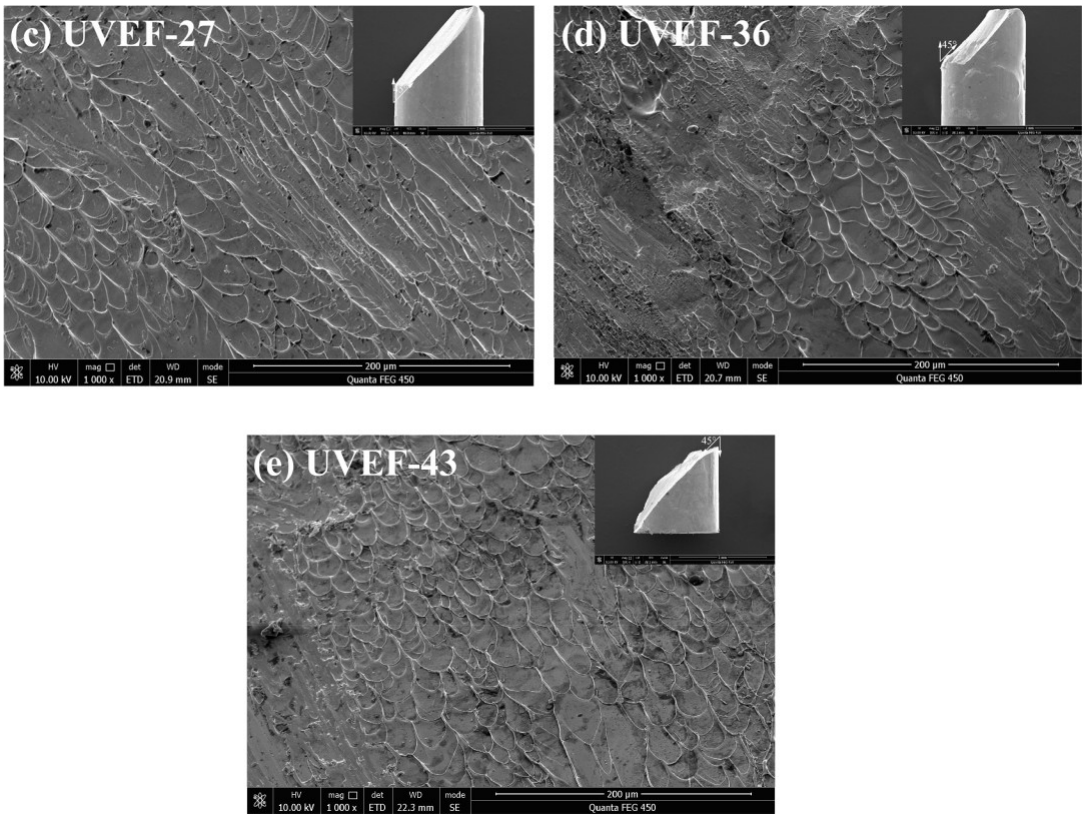


Figure 8. Compressive fracture micromorphology of the as-cast and UVEF-treated samples: (**a**) as-cast; (**b**) UVEF-19; (**c**) UVEF-27; (**d**) UVEF-36; and (**e**) UVEF-43.

Figure 8. Compressive fracture micromorphology of the as-cast and UVEF-treated samples: (**a**) as- (**b**) UVEF-19; (**c**) UVEF-27; (**d**) UVEF-36; and (**e**) UVEF-43.

3.5. Properties of the Hot-Compressed Elastic Deformation Treated Sample

3.5. Properties of the Hot-Compressed Elastic Deformation Treated Sample

From a comparison of XRD patterns of hot-compressed elastic deformation (HEF)-treated samples in Figure 9a, it can be found that the XRD patterns of HEF-treated hot-compressed samples have broad elastic deformation peaks and no obvious crystalline peaks, which can prove that the HEF-treated samples are still have all amorphous broad diffusion. Regarding peaks and the no obvious naming convention, peaks, HEF which-80 refers to amorphous that the HEF samples-treated processed samples by are hot still-compressed all amorphous elastic. Regarding deformation the at sample temperature naming of convention, 80 C. The HEF microscopic-80 refers morphology to amorphous observed samples with processed TEM shown by hot-in-compressed Figure 9b indicates elastic deformation that the HEF at-treated a temperature sample shows of 80 °C a. maze The microscopic-like amorphous morphology structure, observed and no with nanocrystals TEM shown are found in Figure. 9b indicates that the HEF-treated sample shows a maze-like amorphous structure, Figure and 10a no shows nanocrystals the microhardness are found values. of the as-cast and HEF-treated samples. The microhardness value does not decrease with increasing temperature. Compared with the UVEF-treated samples (Figure 7), the e ect of deformation on the amorphous particles is the opposite, indicating that only an elastic deformation treatment with increasing temperature does not induce an increase in the amount of free volume. It is also found that the relaxation enthalpy DH of the HEF-treated sample is slightly larger than that of the as-cast sample (Figure 10b), but as the temperature increases, the relaxation enthalpy DH of the HEF-treated sample essentially does not change, indicating that its free volume does not change with increasing temperature. It also further shows that the aspect of the ultrasonic vibration-assisted elastic deformation process that creates additional free volume is the ultrasonic vibration stress, not the temperature rise caused by the ultrasonic thermal e ect. The ultrasonic vibration stress can create additional free volume and improve the rejuvenation degree of amorphous alloys [31].

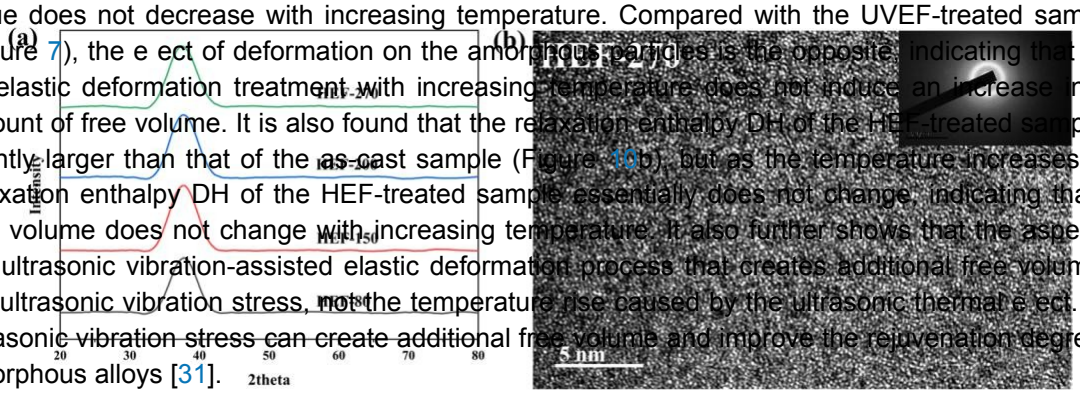
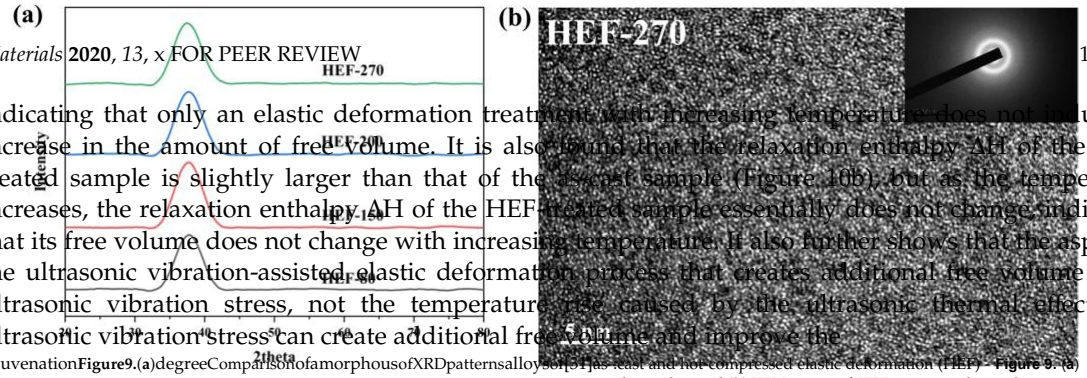


Figure 9. (**a**) Comparison of XRD patterns of as-cast and hot-compressed elastic deformation (HEF) -treated samples, and (**b**) TEM image of HEF-270 treated sample.

Figure 10a shows the microhardness values of the as-cast and HEF-treated samples. The microhardness value does not decrease with increasing temperature. Compared with the UVEF-treated samples (Figure 7), the effect of deformation on the amorphous particles is the opposite,

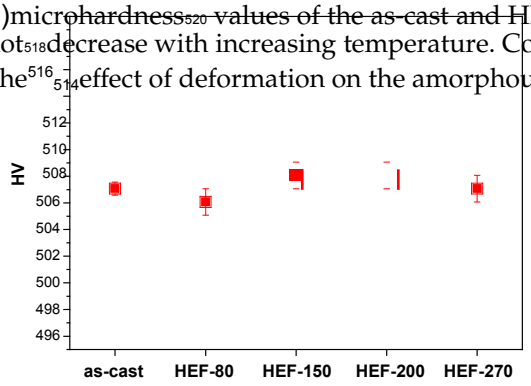
samples in Figure 9a, it can be found that the HEF-treated samples have broad diffusion peaks and no obvious crystalline peaks, which proves that the HEF-treated samples are still all amorphous. Regarding the sample naming convention, HEF-80 refers to amorphous samples processed by hot-compressed elastic deformation at a temperature of 80 °C. The microscopic morphology observed Materials withTEM 2020 shown, 13, 4397 in Figure 9b indicates that the HEF-treated sample shows a maze-like amorphous 11 of 15 structure, and no nanocrystals are found.



indicating that only an elastic deformation treatment with increasing temperature does not induce an increase in the amount of free volume. It is also found that the relaxation enthalpy ΔH of the HEF-treated sample is slightly larger than that of the as-cast sample (Figure 10b), but as the temperature increases, the relaxation enthalpy ΔH of the HEF-treated sample essentially does not change, indicating that its free volume does not change with increasing temperature. It also further shows that the aspect of the ultrasonic vibration-assisted elastic deformation process that creates additional free volume is the ultrasonic vibration stress, not the temperature rise caused by the ultrasonic thermal effect. The ultrasonic vibration stress can create additional free volume and improve the rejuvenation

Figure 9. (**a**) Comparison of XRD patterns of as-cast and hot-compressed elastic deformation (HEF) treated samples, and (**b**) TEM image of HEF-270 treated sample.

Figure 10a shows the (a) microhardness values of the as-cast and HEF-treated samples. The microhardness value does not decrease with increasing temperature. Compared with the UVEF-treated samples (Figure 7), the effect of deformation on the amorphous particles is the opposite,



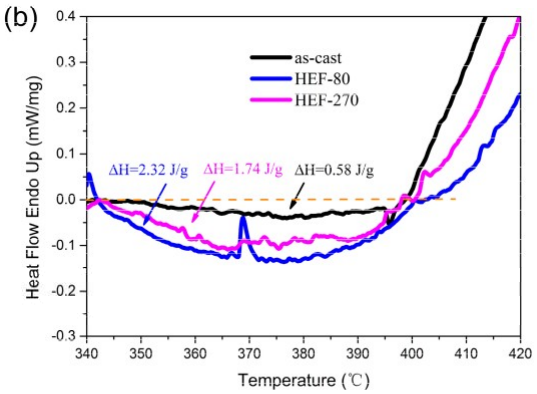


Figure 10. (**a**) Comparison of microhardness of the as-cast and HEF-treated samples and (**b**) comparison of relaxation enthalpies of the as-cast and HEF-treated samples.

It is found that the fracture stress–strain curve of the HEF-treated samples has a very short yield stage before fracture, approximately 0.3% of the strain, and then the samples immediately fracture (Figure 11). At the same time, it is found that the yield strength, elastic modulus, and plastic strain of the HEF-treated sample essentially did not change with increasing temperature. This also verifies the results of Figure 10. The increase in the plasticity of the UVEF-treated sample is caused by an increase in the free volume induced by the ultrasonic vibration stress, which promotes the rejuvenation of the amorphous alloy. The ultrasonic thermal e ect that causes a temperature increase does not increase the plasticity of the amorphous sample. This is because the maximum temperature rise caused by the ultrasonic thermal e ect in this study is 270 C, which is far lower than the T_g of the Zr-based

BMGs. Therefore, at low temperatures, an increase in the temperature cannot increase the free volume. The*Mate*ult*rials*asonic2020 ,vibration*13,x*FORPEERstressREVIEWisthe main reason for the increase in the free volume and the degree12ofof 15 rejuvenation demonstrated herein [31].

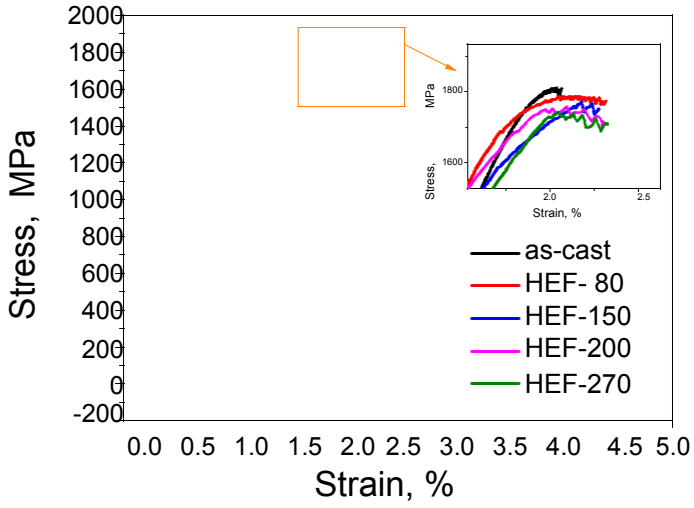


Figure **Figure** **11.** **11** Fracture .Fracture stress stress –strain –strain curve curve ofthe of the as- cast-cast and and HEF HEF -treated -treated samples samples.

3.6. Mathematical Model of the Relationship between Ultrasonic Amplitude And Free Volume

3.6. Mathematical Model of the Relationship between Ultrasonic Amplitude And Free Volume

The shear phase transformation zone (STZ) model [32] is widely used to describe the physical The shear phase transformation zone (STZ) model [32] is widely used to describe the physical process of plastic deformation of amorphous alloy materials. This STZ model is applicable whether the process of plastic deformation of amorphous alloy materials. This STZ model is applicable whether deformation is transient or time-dependent and uniform or nonuniform. Generally, shear deformation the deformation is transient or time-dependent and uniform or nonuniform. Generally, shear is preferentially activated in areas with an increased free volume. Therefore, an increased free volume deformation is preferentially activated in areas with an increased free volume. Therefore, an leads to easier and more shear deformation, which in turn leads to better plasticity. increased free volume leads to easier and more shear deformation, which in turn leads to better It is deduced from this that the BMGs with an increased free volume show a decreased resistance plasticity. to any form of deformation. The ultrasonic amplitude leads to a high-energy state, which increases the It is deduced from this that the BMGs with an increased free volume show a decreased resistance free volume and increases the degree of rejuvenation of amorphous alloys. to any form of deformation. The ultrasonic amplitude leads to a high-energy state, which increases To quantify the e ect of the ultrasonic amplitude on the rejuvenation degree of the amorphous the free volume and increases the degree of rejuvenation of amorphous alloys. samples, the amount of free volume is used to characterize the rejuvenation degree of the amorphous To quantify the effect of the ultrasonic amplitude on the rejuvenation degree of the amorphous alloys, so the amount of free volume in the UVEF-treated samples is theoretically calculated based on samples, the amount of free volume is used to characterize the rejuvenation degree of the amorphous the free volume formula [33]: alloys, so the amount of free volume in the vUVEF-treated samples is theoretically calculated based

$$v_f = v_f \left(\frac{v_f^*}{v_f} \right) \exp\left(\frac{2s\ c}{v_1^{*\ f}} \right) \quad (2)$$

where C is the fitting parameter, v_f is the steady-state free volume, is the shear strain rate, and s is the strain. Also:

$$v_f = \frac{1}{V_{fe}} \quad (k_t \ln + l) \quad (3)$$

$$v_{fe} = \frac{T \quad T_0}{DT_0} \quad (4)$$

where v_{fe} is the equilibrium free volume; k_t = 26.6 + 0.044T and l = 43.9 + 0.082T represent temperature-related parameters [33]; D is the brittleness index of the BMGs, which is taken as 18.5; and T_0 is the Vogel–Fulcher temperature, $T_0 = 2/3T_g$.

The amount of free volume of the UVEF-treated sample can be obtained according to Equation (2), as shown in Figure 12. It can be found that the larger the amplitude of the UVEF-treated sample is, the greater the free volume. Finally, using polynomial fitting, the coe cient of determination for curve

fitting is 0.99983, the mathematical model to obtain the ultrasonic amplitude (A) and free volume (v_f) is obtained as follows:

$$v_f = 7.9857 \ 0.20477A + 0.01216A^2 \quad (5)$$

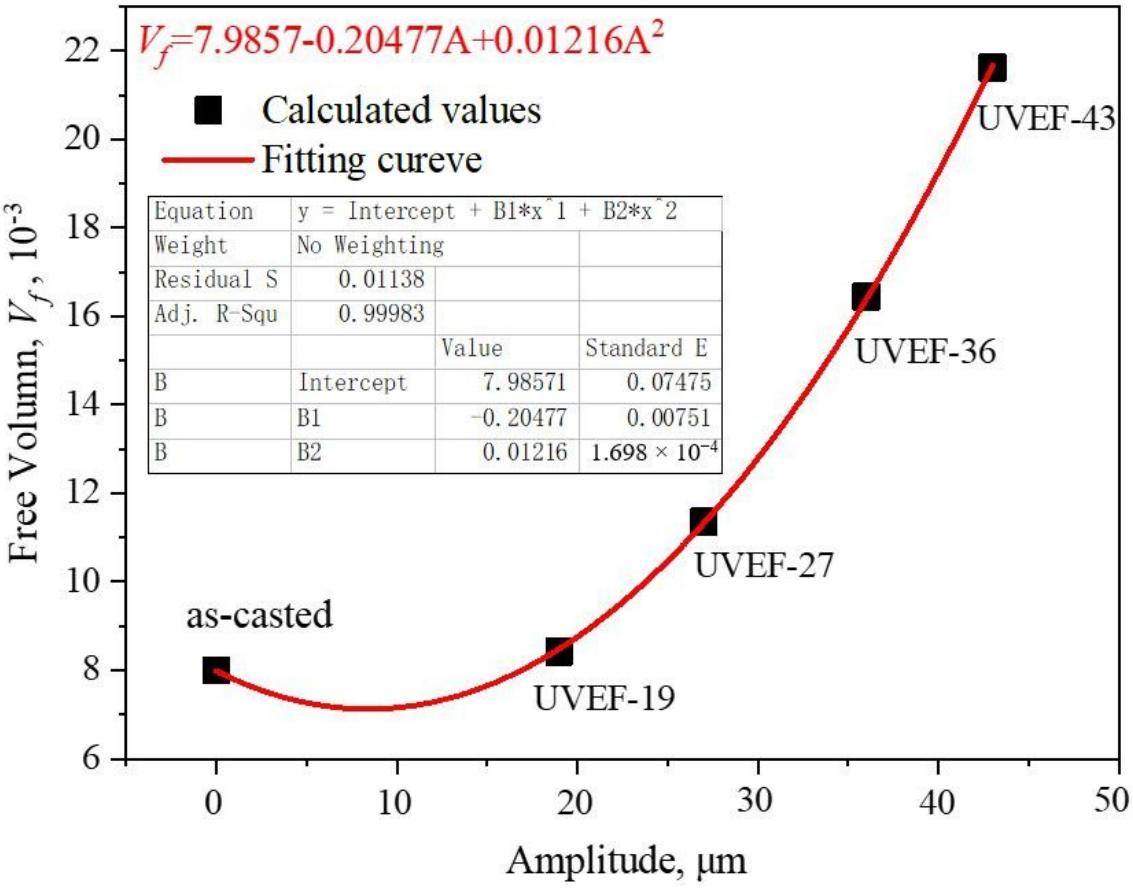


Figure 12. Theoretical model of the relationship between the free volume and amplitude of UVEF-treated samples.

As the amplitude increases, the amount of free volume increases sharply, indicating that the greater the ultrasonic energy is, the greater the degree of amorphous rejuvenation.

4. Conclusions

Compared with metallic glass rejuvenation methods such as elastic loading and ion radiation, UVEF has a short processing time (8s), will not cause damage, and is also controllable. It is found that the relaxation enthalpy increases and the range of the supercooled liquid region decreases when Zr based metallic glasses are UVEF-treated at room temperature. With the increase of amplitude, the free volume and the formability of the UVEF-treated sample increase, and the yield strength and elastic modulus decrease. Ultrasonic vibration stress is the main reason for the increase in the free volume of Zr-based BMGs.

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